

February 15, 2015

Baton Rouge Area Chamber 564 Laurel Street Baton Rouge, LA 70801

Exhibit W. Claiborne Site Preliminary Geotechnical Engineering Report

Attention:

Mr. Jim A. Cavanaugh

Site Development Director

Email:

jim@brac.org

Phone:

(225) 339-1163

Re:

General Geotechnical Site Characterization Report

Claiborne Plantation Iberville Parish, Louisiana PSI Project No. 0254771

Dear Mr. Cavanaugh:

Professional Service Industries, Inc. is pleased to submit this General Geotechnical Site Characterization Report for the Claiborne Plantation Site Study. This report includes the results of field and laboratory testing, and information regarding the compatibility of this site with industrial development, suitability of soils for building foundations and on-site roadways, requirements of soil augmentation for construction of a typical 100,000 square feet (sf) industrial manufacturing building and depth of groundwater.

We appreciate the opportunity to perform this Preliminary Geotechnical Site Evaluation Report. If you have any questions pertaining to this report, or if we may be of further service, please contact our office.

Respectfully submitted,

PROFESSIONAL SERVICE INDUSTRIES, INC.

Nicholas K. Miller, P.E.

Project Engineer

Geotechnical Services

Reda M. Bakeer, Ph.D., P.E. Senior Vice President

Name: Nicholas K. Miller, P.E.

Date: February 15, 2016

License No.: 40111

THIS PRELIMINARY DOCUMENT IS NOT TO BE

USED FOR CONSTRUCTION, BIDDING,

RECORDATION, CONVEYANCE, SALES, OR AS THE BASIS FOR THE ISSUANCE OF A PERMIT.



GENERAL GEOTECHNICAL SITE CHARACTERIZATION REPORT

CLAIBORNE PARISH SITE IBERVILLE PARISH, LOUISIANA PSI PROJECT NO.: 0254771

PREPARED FOR

BATON ROUGE AREA CHAMBER 564 LAUREL STREET BATON ROUGE, LA 70801

FEBRUARY 15, 2015

BY
PROFESSIONAL SERVICE INDUSTRIES, INC.
11950 INDUSTRIPLEX BLVD.
BATON ROUGE, LOUISIANA 70809

TABLE OF CONTENTS

Page No.
PROJECT INFORMATION
SITE AND SUBSURFACE CONDITIONS 2 Site Location and Description 2 Site Geology 2 Field Exploration 2 Laboratory Testing 3 Subsurface Conditions 3 Groundwater Information 4 Seismic Design Considerations 4
EVALUATION AND DISCUSSIONS5
REPORT LIMITATIONS
APPENDIX
 Site Vicinity Map Boring Location Plan Boring Logs Key to Terms and Symbols Used on Logs

PROJECT INFORMATION

Project Authorization

Professional Service Industries, Inc. (PSI) has completed a General Geotechnical Site Study at the Claiborne Plantation site, located in Iberville Parish, Louisiana. Our services were provided in general accordance with PSI Proposal No. 254-155351, dated June 23, 2015. Authorization to provide our services was provided by Mr. Kyle Zeringue (Senior Vice President, Business Development, Baton Rouge Area Chamber) who signed our Proposal on January 6, 2016.

Project Description

The primary objectives for this preliminary report are to provide general information regarding the compatibility of this site with industrial development, suitability of soils for building foundations and on-site roadways, requirements of soil augmentation for construction of a typical 100,000 square feet (sf) industrial manufacturing building, and the depth of free groundwater table. This genera geotechnical site characterization report will provide an initial baseline of the site subsurface conditions that will likely be encountered during future site development. However, as with any geotechnical investigation, particularly given the size of this subject site and the relatively limited number of borings performed, variations between borings may and should be expected to exist, and there remains a distinct possibility that other conditions may exist on site that were not encountered within the scope of this exploration.

The opinions and information to be presented in this report are estimates for preliminary consideration only, are based on limited geotechnical exploration, and are not to be used for final design and construction. A detailed geotechnical exploration and analyses should be performed once design and function of the proposed development have been finalized.

Purpose and Scope of Services

The purposes of PSI's geotechnical services are to:

- Perform 5 soil borings at the site per the request of the Client;
- Evaluate general subsurface soil conditions and groundwater depth at the subject site;
- Perform limited laboratory testing on selected soil samples recovered from the borings; and.
- Provide a general discussion regarding the compatibility of this site with industrial development, suitability of soils for building foundations and on-site pavement improvement, and requirements of soil augmentation for construction of a typical 100,000 square foot industrial manufacturing building.

The scope of services did not include an environmental assessment for determining the presence or absence of wetlands, or hazardous or toxic materials in the soil, surface water, groundwater, or air on or below, or around this site. Any statements in this report or on the boring logs regarding odors, colors, and unusual or suspicious items or conditions are strictly for informational purposes. Prior to development of this site, an environmental assessment is advisable. Additionally, PSI did not provide any service to investigate or detect the presence of moisture, mold or other biological contaminants in or around any structure, or any service that was designed or intended to prevent or lower the risk of the occurrence or the amplification of the same. Client acknowledges that mold is ubiquitous to the environment with mold amplification occurring when building materials are impacted by moisture. Client further acknowledges that site conditions are outside of PSI's



control, and that mold amplification will likely occur, or continue to occur, in the presence of moisture. As such, PSI cannot and shall not be held responsible for the occurrence or recurrence of mold amplification.

SITE AND SUBSURFACE CONDITIONS

Site Location and Description

The subject site is approximately 1,050 acres in size and is located on the south side of LA Highway 405 beginning approximately 1½ mile east of its intersection with Cannonburg road and extending 1½ miles to the Iberville/Ascension Parish line in White Castle, Iberville Parish, Louisiana. The site extends southward approximately 2 miles from the LA Highway 405. It is bound by LA Highway 405 to the north and elsewhere by mostly undeveloped, rural/agricultural land. The site is currently used primarily for agricultural purposes and contains several dirt and gravel access farm roads. The site also contains several developments including a residential structure, silos, and farm equipment storage barns. Several ditches and other runoff conveyances were observed during our field reconnaissance.

PSI's truck-mounted and ATV-mounted drill rigs were used to perform this field exploration. The truck-mounted drill rig experienced difficulty traversing the site over the existing farm roads within a few days of rain events and was subsequently replaced with a track-mounted drill rig. All of the borings were located just off of existing field roads. PSI made no attempt to enter the cultivated portions of the site.

Site Geology

Based on the Geological Map of Louisiana (1984), the site is located within the Natural Levees Formation (Qnl) geologic unit. The Natural Levees geologic unit is characterized by gray and brown silt and silty clay with some very fine sand. Per the U.S. Geological Society (USGS), these deposits are encountered on past and present courses of major streams. Natural Levee deposits in the site vicinity are relatively weak and compressible in nature. A drainage or seepage drainage feature is located in the western portion of the site.

Field Exploration

The field exploration included mobilization to the site by a PSI drilling crew, drilling of the soil borings, and recovering soil samples from the soil borings. Borings B-1 and B-5 were extended to a depth of approximately 40 feet below the existing ground surface. Borings B-2 and B-4 were extended to a depth of about 20 feet below the existing ground surface. Boring B-3 was extended to a depth of approximately 80 feet below existing grade. Refer to the Boring Location Plan given in the Appendix for the approximate boring locations.

Drilling and sampling activities were performed in general accordance with referenced ASTM procedures or other accepted methods. The boreholes were backfilled with a cement/bentonite grout mixture per LADOTD and LDEQ requirements.

Undisturbed samples of cohesive soils were generally obtained using three-inch-diameter, thin-wall tube samplers (Shelby tube) in general accordance with the procedures for "Thin-Walled Tube Geotechnical Sampling of Soils" (ASTM D1587). These samples were extruded in the field with a hydraulic ram and were identified according to boring number and depth, wrapped in



aluminum foil, placed in polyethylene plastic wrapping to protect against moisture loss and transported to the laboratory in containers to minimize disturbance.

For cohesionless soils, Standard Penetration Tests (SPT) were performed to obtain standard penetration values of the soil using a 140-pound hammer, falling 30 inches. The test is performed by lowering the standard penetrometer sampler to the bottom of the previously cleaned drill hole and advanced by blows from the hammer. The number of blows is recorded for each of the three consecutive 6-inch increments. The "SPT-N" value is obtained by adding the second and the third incremental numbers. The results of the standard penetration test indicate the relative density of cohesionless soils, and thereby provide a basis for estimating the relative strength and compressibility of the soil profile components. Soil samples were obtained utilizing a two-inch O.D. split-barrel sampler in general accordance with procedures for "Penetration Test and Split-Barrel Sampling of Soils" (ASTM D 1586). These samples were also identified according to boring number and depth, placed in polyethylene plastic wrapping to protect against moisture loss and transported to the laboratory.

Laboratory Testing

Selected soil samples were tested in the laboratory to determine material properties for our evaluation. Visual classifications were performed in the laboratory. Physical testing included determination of moisture contents, Atterberg limits classification testing and unconfined compressive strength or unconsolidated undrained triaxial shear tests to supplement the field pocket penetrometer and torvane testing. The laboratory testing was performed in general accordance with ASTM standard procedures. Samples not altered by laboratory testing will be retained for sixty days from the date of this report and then be discarded.

Subsurface Conditions

Boring B-1 encountered very soft to stiff lean and fat clay to a depth of about 22 feet below the existing ground surface (bgs). A relatively thin loose silty sand stratum was encountered beneath the clay followed by a thin stratum of firm fat clay. Loose, poorly graded sand was encountered below a depth of about 27 feet bgs to the terminal depth of the boring of 40 feet.

Borings B-2 and B-4 generally encountered firm to very stiff lean (only in B-4) and fat clay soils to the terminal depth of 20 feet bgs.

Boring B-3 encountered firm to stiff lean and fat clay soils to a depth of about 8 feet bgs. These soils were underlain by a very loose to loose sand stratum extending from about 8 to 25 feet bgs. Soft to firm lean and fat clay soils were encountered beneath the sand to a depth of around 62 feet bgs. Silt with sand and clay was generally present below that depth to the terminal depth of the boring at 80 feet; however, a thin statum of medium dense sand was encountered between about 73 and 75 feet bgs within this silt interval.

Boring B-5 generally encountered soft to very stiff fat clay to a depth of about 32 feet bgs which is underlain by a thin stratum of firm lean clay with sand followed by silty clayey sand to the terminal depth of the boring at about 40 feet. The upper clay soils were stiff to very stiff and transitioned to a soft to firm consistency beneath about 8 feet bgs. The relative density of the silty clayey sand encountered at around 38 feet bgs would be considered loose to medium dense.



The above subsurface description is generalized in nature to highlight the major subsurface stratification features and material characteristics. The boring logs included in the Appendix should be reviewed for specific information at the individual boring locations. These records include soil descriptions, stratifications, penetration resistances, locations of the samples, and laboratory test data. The stratifications shown on the boring logs represent the conditions only at the actual boring locations. Variations may occur and should be expected between boring locations. The stratifications represent the approximate boundary between subsurface materials and the actual transition may be gradual. This is particularly important considering the site size and the limited number of borings performed which were all performed within the immediate vicinity of the existing farm roads.

Groundwater Information

Groundwater was encountered in four of the five borings during the exploration. The groundwater depth measured in the borings during our drilling activities are shown in the following table.

Table 1: Groundwater Depth Measured During Drilling

Boring	Groundwater Depth During Drilling (feet below the existing ground surface)									
B-1	12									
B-2	16									
B-3	10									
B-4	16									
B-5	Not Encountered									

It should be noted that groundwater level fluctuations at this site may occur due to seasonal and climatic variations, the stage of the Mississippi River due to its relative close proximity to the subject site, alteration of drainage patterns, land usage and ground cover. Additionally, perched water may be encountered in discontinuous zones within the overburden. This condition develops as rainwater in entrapped in the more pervious surface cultivated soils underlain by less pervious cohesive soils. We recommend the Contractor determine the actual groundwater levels at the time any future construction activities begin.

Seismic Design Considerations

The design of structures must consider dynamic forces resulting from seismic events. These forces are dependent upon the magnitude of the earthquake event as well as the properties of the soils that underlie the site. As part of the procedure to evaluate seismic forces, the evaluation of the Seismic Site Class, which categorizes the site based upon the characteristics of the subsurface profile within the upper 100 feet of the ground surface, is required. To define the Site Class for this site, we have interpreted the results of soil test borings drilled within the subject site and estimated appropriate soil properties below the base of the borings to a depth of 100 feet as permitted by the International Building Code, 2012 edition. The estimated soil properties were based upon our experience with subsurface conditions in the general site area. Based upon our evaluation, the subsurface conditions within the site are consistent with the characteristics of a Site Class "E" as defined in Table 20.3-1 of the ASCE Standard 7-10. This assessment can and should be better defined by performing additional deep borings and associated geotechnical laboratory testing.



Iberville Parish, Louisiana

EVALUATION AND DISCUSSIONS

The type and depth of foundation suitable for a given structure primarily depends on several factors including the subsurface conditions, the function of the structure, the loads it may carry, the cost of the foundation and the criteria set by the Design Engineer with respect to vertical and differential movements which the structure can withstand without damage. Detailed column loads for a typical 100,000 sq. ft. industrial manufacturing building were not provided at the time of this study; however, the structural column loads are anticipated to be on the order of 100 kips, with wall loads on the order of about 5 kips per lineal foot. Grading plans are also not available at this time; although, we anticipate fill material on the order of about 4 feet may be required to achieve final grades. The proposed designs should also consider the requirements of the U.S. Army Corps of Engineers (USACE) with regard to any construction to be made within 1,500 feet from the existing flood protection structure along the adjacent Mississippi River.

Again, it should be noted that the exploration locations were performed on or near the shoulder of existing farm roads. No attempt was made to enter cultivated areas typically used for planting crops. It should be assumed that the upper soils encountered in the cultivated areas will require significantly more effort to achieve proper compaction and may contain far more organic material and other additives (fertilizers, etc.) in the upper soils than the areas explored during this preliminary exploration.

The choice of type of deep foundation should be based on the tolerance criteria for the performance of the structures and economics of construction. Grade supported foundations or surface coverings will likely be governed by the anticipated load and settlement tolerances, particularly where a significant amount of new fill is placed. Driven piles should be viable foundation types considering the subsurface and groundwater conditions encountered and should be anticipated to carry the structural loads anticipating that settlement will occur as a result of new fill, building and slab loads. As previously discussed, construction in some areas of the site will be subjected to review and approval of the USACE. Lightly-loaded equipment pads may be able to be supported on shallow spread footings, or mat foundations, as long as the PVR issues described below are mitigated and settlement potential considered. Prior to new fill placement, site preparation should include removal of surficial topsoil, organic materials, and soft soil or demucking of wet areas or drainage conveyances and proofrolling in the presence of the Geotechnical Engineer to assess general stability and firmness prior to fill placement.

Based on the limited number of soil borings, field data and laboratory test results, the proposed site is generally feasible for industrial development. The subsurface soils explored are suitable for building foundations and site roadways after proper preparation. Fat clay soils with high shrink/swell potential (Plasticity Indices ranging from 29 to 61) were encountered near the ground surface (upper 8 feet) across the site. Potential Vertical Rise (PVR) should be further evaluated considering new fill that may be placed at the site to achieve final grades. PVR in portions of this site could be mitigated by undercutting the fat clay soils to a predetermined depth and replacing with moisture-conditioned, properly compacted lean clay (CL) soils, or with the addition of chemical treatment such as lime mixing. Based on the anticipated new fill thickness on the order of around 4 feet, PVR is not anticipated to adversely impact the project with great significance. The effects of PVR should be considered if lesser fills are planned. The suitability of reuse of excavated soils (ponds, etc.) as structural fill may require the use of lime treatment or soil mixing.



Site pavements should be underlain by at least 12 inches of properly compacted low plasticity engineered fill material or otherwise or chemically treated with lime prior to base material placement due to the near surface fat clay soils. At this time, we assume pavement areas will receive at least two to four feet of fill to achieve final grades.

Areas within 1,500 feet of the existing levee to the north of the site should anticipate USACE interaction per the Hurricane and Storm Damage Risk Reduction System (HSDRRS) Design Guidelines and will likely be subject to the requirements of the Lower Mississippi Valley (MVN) and New Orleans District (NOD) requirements. Special permitting should also be anticipated for any geotechnical borings, new fill or excavations, and any loading or changes in loading configurations within the referenced area of the site. Supplemental exploration and sampling methods, laboratory testing and engineering analysis (including, but not limited to, slope stability, seepage analysis, and settlement analysis) following the HSDRRS Design Guidelines may be required for the project. Additionally, the USACE permits typically prohibit excavation or deep foundation installation during periods of high water (typically late April through late July but may vary dependent on the weather conditions in the region) as detailed by the permit requirements. Strict monitoring of pile driving is also mandated by the USACE in terms of vibration and potential impact on the adjacent flood protection system.

As stated previously, PSI's opinions and information presented in this site evaluation report are provided for planning purposes and preliminary considerations only; they are based on a very limited geotechnical exploration, and are not to be used for final design and construction.

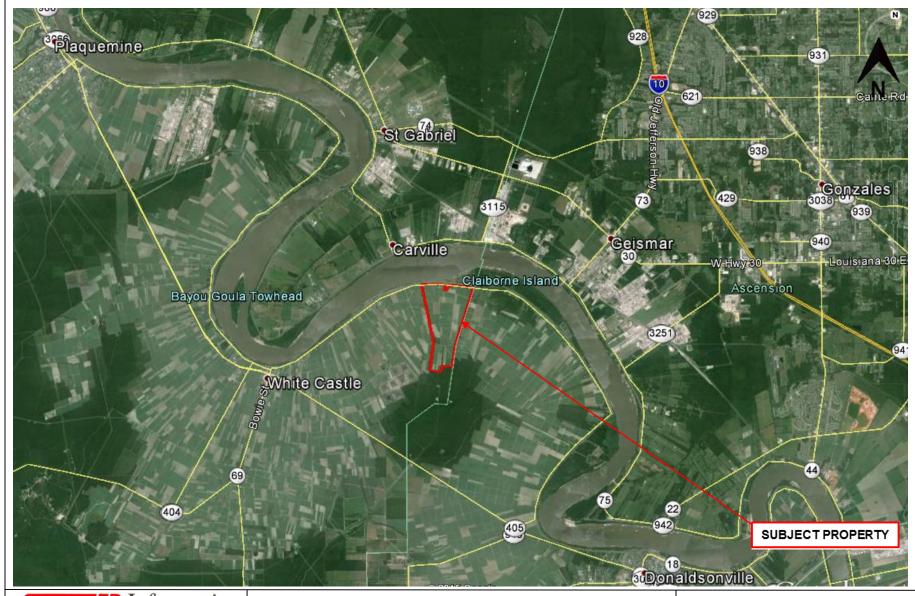
REPORT LIMITATIONS

The preliminary information submitted in this report is based on the available subsurface data obtained by PSI at the time of our field exploration. PSI warrants that the preliminary findings contained herein have been made in accordance with generally accepted drilling procedures and visual soil classification methods in the local area. No other warranties are implied or expressed. This report has been prepared for the exclusive use of the Baton Rouge Area Chamber for the specific purpose of determining general subsurface information at the subject site to develop a general geotechnical site characterization.



APPENDIX







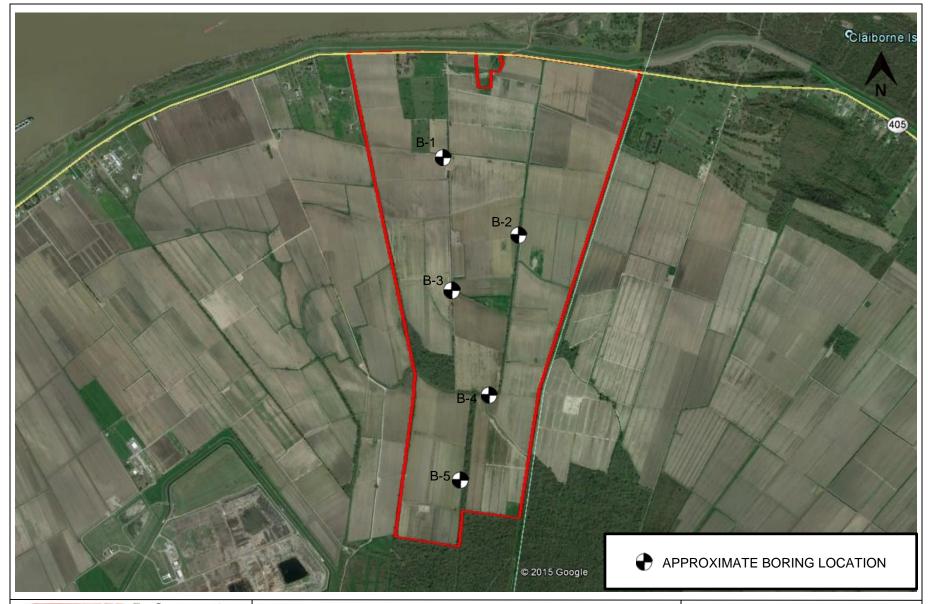
SITE VICINITY MAP

PSI PROJECT NO.: 0254771

GEOTECHNICAL SITE CHARACTERIZATION

CLAIBORNE PLANTATION

IBERVILLE PARISH, LOUISIANA





BORING LOCATION PLAN

PSI PROJECT NO.: 0254771

GEOTECHNICAL SITE CHARACTERIZATION

CLAIBORNE PLANTATION

IBERVILLE PARISH, LOUISIANA

CLAIBORNE PLANTATION LA HIGHWAY 405 IBERVILLE PARISH, LOUISIANA

TYP	TYPE OF BORING: WET ROTARY					LOCA	TION	: BUI	LDIN	G ARI	EA	PSI Project No.: 0254				
ا ا				Τ.	@			<u></u>	ćΨ.	SHEAR STRENGTH (tsf)	s	SH	EAR GTH (ts	f)	IGHT	
TH, FT.	SOIL TYPE	USCS SYMBOL	SAMPLES		N-BLOWS/FT.	MOISTURE CONTENT (%)	LIQUID	PLASTIC	PLASTICITY INDEX	% PASSING No. 200 SIEVE	O HP ● UC			IE (tsf)		UNIT DRY WEIGHT (pcf)
DEPTH,	SOII	SCS	SAI	SOIL DESCRIPTION	N-BL	CON		_	립	% P/ No. 20	△ TV ▲ UU 0.0 0.5 1.0 1.5	HAND PEN (tsf)	UC (tsf)	TORVANE (tsf)	UU (tsf)	NIT
		CL	$\frac{1}{2}$	Stiff gray LEAN CLAY , with gravel and	12	22	LL	PL	PI		0.0 0.3 1.0 1.3			2		
- 2.5-			$\frac{X}{A}$	shell fragments (POSSIBLE FILL)												
		СН	X	Soft to firm gray FAT CLAY , with silt and	16	10						0.00	0.00			
- 5.0-				sand seams		31	F.4	00	00			0.33	0.38			86
- 7.5 -						33	51	22	29			0.25				
-10.0-						35								0.25		
- 12.5				$\bar{\Delta}$												
						33								0.15		
- 15.0 -																
- 17.5 -		_CH		Very soft gray FAT CLAY , with sand layers												
-20.0-				,		44							0.11	0.20		76
00.5		SM		Lacco grov CH TV CAND												
-22.5		SIVI	\forall	Loose gray SILTY SAND	5	29				21						
25.0		СН	4	Firm gray FAT CLAY , with sand seams												
- 27.5		SP-SN	1	Loose gray SAND with silt												
-30.0						63					19		0.34	0.25		67
-32.5					6	23				8						
35.0			4		0	25										
37.5																
0 40 0			X		9	22				9						
40.0				Boring terminated at 40 feet												
42.5																
45.0																
ያ ዘ-47.5•																
50.0				10 40 5557												
ار	IH O E DR			NG: 40 FEET 1/19/16							UNDWATER DURI					

NOTE:

CLAIBORNE PLANTATION LA HIGHWAY 405 IBERVILLE PARISH, LOUISIANA

TYPE OF	BOR	INC	G: SOLID STEM AUGER		LOCA	TION	: BUI	LDIN	G ARE	Α	F	PSI Pro		lo.: 02	54771
DEPTH, FT.	USCS SYMBOL	SAMPLES	SOIL DESCRIPTION	N-BLOWS/FT.	MOISTURE CONTENT (%)	LIQUID	PLASTIC LIMIT	PLASTICITY INDEX	% PASSING No. 200 SIEVE	SHEAR STRENGTH (tsf) ○ HP ● UC △ TV ▲ UU 0.0 0.5 1.0 1.5	HAND PEN (tsf)	SHI C (tst) C (tst)	ORVANE (tsf) HYS	UU (tsf)	UNIT DRY WEIGHT (pcf)
	CH	М	Stiff gray FAT CLAY, with gravel and	10	27	<u>LL</u> 64	PL 20	PI 44					Τ		ر
-2.5-	Ch		shell fragments (POSSIBLE FILL) Firm to stiff gray FAT CLAY		32					-	0.67	0.82			 90
-5.0-					30						1.00	0.02			30
3.0					33						0.50				
-7.5			-silt and sand seams and gravel, 8 to 10				0.5								
10.0			feet -trace organic, 8 to 15 feet		34	86	25	61			0.67				
12.5															
					36						0.50	0.32			84
-15.0-			$ar{\Sigma}$												
17.5			-sand seams, below 18 feet												
20.0			Boring terminated at 20 feet		39								0.30		
-22.5			Borning terminated at 20 leet												
22.5															
- 25.0 -															
- 27.5 -															
- 30.0 -															
-32.5 -															
-35.0-															
১ -37.5															
81 91/91 -40.0 -															
2															
9. -42 .5 -															
-42.5- -45.0-															
2 47.5=															
NROUC															
-47.5- -50.0-			WO 00 FFFT												
S DELLH C			NG: 20 FEET 1/19/16							JNDWATER DURII UNDWATER UPON					
DATE DF NOTE:										YED GROUNDWA			71	•	

CLAIBORNE PLANTATION LA HIGHWAY 405 IBERVILLE PARISH, LOUISIANA

TYPE	TYPE OF BORING: WET ROTARY				1	LOCA	TION	: BUI	LDIN	G ARI	EA	F		oject N	lo.: 02	
FT.	ш	BOL	S		l H	(%		O		S H	SHEAR STRENGTH (tsf)	s	SH TREN	IEAR IGTH (ts	sf)	UNIT DRY WEIGHT (pcf)
	SOIL TYPE	USCS SYMBOL	SAMPLES		N-BLOWS/FT.	MOISTURE CONTENT (%)	LIQUID	PLASTIC LIMIT	PLASTICITY INDEX	% PASSING No. 200 SIEVE	○ HP ● UC	6	_	(tsf)	(J)	Y WE
DEPTH,	OIL	CS 8	SAM	SOIL DESCRIPTION	BLO	MOIS		P	PLA	6 PA	△ TV ▲ UU	HAND PEN (tsf)	C (tsf	/ANE	UU (tsf)	DR,
	S	NS		SOIL DESCRIPTION	Ż	_ Ö	LL	PL	PI	°ž	0.0 0.5 1.0 1.5	ᄪ	Ď	TORVANE (tsf) H	٦	N N
		CL		Firm brown LEAN CLAY with root fibers and sand (POSSIBLE FILL)		14						1.50				
-2.5-		СН		Firm to stiff brown FAT CLAY with silt		27	53	18	35					0.30	0.32	90
- 5.0 -						23	53	18	35			1.17				
5.0							33	10	33			1.17				
- 7.5		SP	Х	Variables to leave grow CAND	4	27				59						
-10.0-		31	X	Very loose to loose gray SAND	2	31										
10.0				_												
-12.5																
- 15.0 -			X		2	33										
10.0																
- 17.5 -																
-20.0-			X		WOH	34										
20.0																
-22.5																
- 25.0 -	7777		X		6	34										
		CL		Firm gray LEAN CLAY with trace sand												
- 27.5 -																
-30.0-						47	37	20	17	99				0.30	0.24	81
- 32.5 -																
-35.0-			X		2	44										
. 025																
-37.5 -																
-37.5 -						39								0.25		
DT - 2																
9-42.5																
-42.5- -45.0-						38								0.40		
- PSI																
병 -4 7.5 -		СН		Soft to firm gray sandy FAT CLAY												
BATONROUGE -50.0-						30	64	23	41	52				0.15		
	TH O	F BO	⊥ RII	NG: 80 FEET		<u> </u>	I	I	∇	GPO	UNDWATER DURI	NG DD		3: 10 ==		<u> </u>
()				2/9/16							UNDWATER UPO					
NOTI	Ξ:								Ţ	DELA	AYED GROUNDWA	ATER: N	N / A			

CLAIBORNE PLANTATION LA HIGHWAY 405 IBERVILLE PARISH, LOUISIANA

		G: WET ROTARY		LOCA	TION	: BUI	LDIN	G ARI	EA	PS	I Project	No.: 02	
DEPTH, FT. SOIL TYPE	USCS SYMBOL SAMPLES		N-BLOWS/FT.	MOISTURE CONTENT (%)	LIQUID	PLASTIC LIMIT	PLASTICITY INDEX	% PASSING No. 200 SIEVE	SHEAR STRENGTH (tsf) ○ HP ● UC	STI	UC (tsf) BASANCE (tst) HASANCE	(tsf)	UNIT DRY WEIGHT (pcf)
SOIL	USCS	SOIL DESCRIPTION	N-BL(CONT	LL	PL	PI	% P/ No. 20	△ TV ▲ UU 0.0 0.5 1.0 1.5	HAND PEN (tsf)	UC (ts	UU (tsf)	UNIT DE
-52.5	X		4	34									
-55.0 -57.5													
60.0-				52							0.2	0.35	73
	МН	Firm gray SILT with sand and clay		26						0.33			
-65.0- -67.5-													
-7 0.0 -	X		5	38				68					
	C-SM	Medium dense gray Sand with clay and silt	16	29				35					
-75.0- -77.5- III N	MH	Medium dense gray SILT with sand											
80.0	X	and clay	10	32				81					
-82.5 -		Boring terminated at 80 feet											
- 85.0 -													
87.5													
07.5													
90.0-													
92.5													
95.0													
97.5													
92.5- 95.0- 97.5- 100.0- DEPTH OF DATE DRIL													
DEPTH OF		NG: 80 FEET											
DATE DRIL	LED:	2/9/16											

CLAIBORNE PLANTATION LA HIGHWAY 405 IBERVILLE PARISH, LOUISIANA

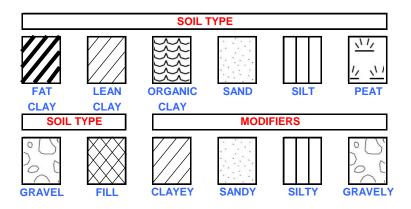
TYP	TYPE OF BORING: SOLID STEM AUGER					LOCA	OCATION: BUILDING AREA							PSI Project No.: 025477			
H.	ш	BOL	S		l H	ш [©]		U	È.	G VE	SHEAR STRENGTH (tsf)	s	SH TREN	EAR GTH (ts	sf)	IGHT	
DEPTH, F	SOIL TYPE	USCS SYMBOL	SAMPLES	SOIL DESCRIPTION	N-BLOWS/FT.	MOISTURE CONTENT (%)	LIQUID	PLASTIC	PLASTICITY INDEX	% PASSING No. 200 SIEVE	O HP ● UC △ TV ▲ UU	HAND PEN (tsf)	IC (tsf)	日 日 TORVANE (tsf)コロス	UU (tsf)	UNIT DRY WEIGHT (pcf)	
	0,					0	LL	PL	PI	z z	0.0 0.5 1.0 1.5	_ H	ר	TOR		Š	
		CL	M	Very stiff brown LEAN CLAY with sand	8	19											
-2.5-						17	43	17	26	83		1.50					
- 5.0-						17						1.41					
- 7.5 -			M		5	28				88							
		СН		Firm Gray FAT CLAY		49	81	21	60					0.20	0.38	75	
- 10.0																	
-12.5																	
						39								0.25			
- 15.0				$ar{ abla}$													
- 17.5				_													
17.0			Ħ			34	75	21	54					0.30	0.48	86	
-20.0				Boring terminated at 20 feet													
-22.5																	
22.5																	
-25.0											 						
27.5																	
- 27.5																	
-30.0																	
-32.5																	
35.0	-																
- 0254																	
5.78 -	-																
0.0 4	1																
- 1	- 1																
-42.5 -45.0																	
OUST																	
9 4 5.0																	
병 47.5	<u> </u>																
NRO																	
-50.0																	
g DEF	тно			NG: 20 FEET							UNDWATER DURI						
NOT DAT		ILLEI	J. 1	2/9/16							UNDWATER UPON YED GROUNDW <i>A</i>			ON: 14	1/2 FE	ET	
ы П									¥	DLLP	TIED GIVOUNDWA	VILIN. I	1 / / 1				

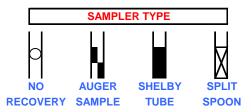


CLAIBORNE PLANTATION LA HIGHWAY 405 IBERVILLE PARISH, LOUISIANA

SHEAR STRENGTH (sb)	TYP	TYPE OF BORING: WET ROTARY					LOCA	TION	: BUI	LDIN	G ARI	EA	F	54771			
CH Stiff to very stiff brown FAT CLAY with trace all and organic		Ш	BOL	S		l H	ш (%		U	<u>`</u>	ر رو	SHEAR STRENGTH (tsf)	STRENGTH (tsf)				IGHT
CH Stiff to very stiff brown FAT CLAY with trace all and organic		TYP	SYM	PLE		WS/F	ENT (JIMI-	ASTI IMIT	STIC	SSIN SSIN	O HP ● UC			E (tsf)		Y WE
CH Stiff to very stiff brown FAT CLAY with trace all and organic	EPT	OIL	CS 8	SAIV	SOIL DESCRIPTION	-BLO	MOIS		4	PLA =	% PA 0. 200	△ TV ▲ UU	IAND EN (ts	C (ts)	VANE	JU (ts	T DR
CH Soft to very stiff brown FAT CLAY with trace sit and organic 18 19 61 20 41 92 1.25 1.42 1.25 1.32 100 1.55 1.50 1.50 1.50 1.50 1.50 1.50		0)	NS			Z	-ō	LL	PL	PI	°`ž	0.0 0.5 1.0 1.5	고핆	n	TOR	٦	N N
25 19 61 20 41 92 1.25 1.32 100 7.5- CH Soft to firm gray FAT CLAY with trace silt trace organic, 8 to 10 feet 23 1.25 1.32 100 12.5- 1.50 1.50 1.50 1.50 1.50 1.50 17.5- 20.00 22.5- 25.00 2.50 1.50 1.50 27.5- 20.00 22.5- 25.00 2.50 2.50 28.5- 20.00 22.5- 25.00 2.50 2.50 28.5- 20.00 20.00 20.00 20.00 28.5- 20.00 20.00 20.00 20.00 28.5- 20.00 20.00 20.00 28.5- 20.00 20.00 20.00 28.5- 20.00 20.00 20.00 28.5- 20.00 20.00 20.00 28.5- 20.00 20.00 20.00 28.5- 20.00 20.00 20.00 28.5- 20.00 20.00 28.5- 20.00 20.00 28.5- 20.00 20.00 28.5- 20.00 20.00 28.5- 20.00 20.00 28.5- 20.00 20.00 28.5- 20.00 20.00 28.5- 20.00 20.00 28.5- 20.00 20.00 28.5- 20.00 20.00 28.5- 20.00 20.00 28.5- 20.00 20.00 28.5- 20.00 20.00 28.5- 20.00 20.00 28.5- 20.00 20.00 28.5- 20.00 28.5- 20.00 20.00 28.5- 20.0			СН		Stiff to very stiff brown FAT CLAY with		18						1.42				
24	- 2.5-			H	nace on and organic		10	61	20	11			1 42				
25				H			19	01	20	4'			1.42				
CH Soft to firm gray FAT CLAY with trace silt trace organic, 8 to 10 feet 12.5 18 37	- 5.0-						24				92		1.25			1.32	100
CH solf to firm gray FAT CLAY with trace slit trace organic, 8 to 10 feet 12.5 15.0 17.5 20.0 17.5 20.0 18.0 19.	- 7.5						25						0.92				
trace organic, 8 to 10 feet 12.5			СН				23						0.50				
115.0 117.5 117.5 120.0	-10.0			-	trace organic, 8 to 10 feet												
115.0 117.5 117.5 120.0	12.5																
11.5.0 11.5.0 11.5.0 11.5.0 11.5.0 12.0 12.5.0	12.3						34	55	18	37					0.45		
22.0- 22.5-	-15.0			H			•								0.10		
22.0- 22.5-																	
22.5. 23.5. 24.0. 25.0. 26.0. 26.0. 27.5. 26.0. 27.5. 26.0. 27.5. 27.5. 28.0. 28	17.5			H											0.55		
27.5 30.0 27.5 30.0 32.5 CL Firm gray LEAN CLAY with sand 33 40 20 20 85 37.5 SC-SM Medium dense gray SILTY CLAYEY SAND 10 35 31 Boring terminated at 40 feet 7 GROUNDWATER DURING DRILLING: NOT ENCOUNTER	-20.0						51								0.55		
27.5 30.0 27.5 30.0 32.5 CL Firm gray LEAN CLAY with sand 33 40 20 20 85 37.5 SC-SM Medium dense gray SILTY CLAYEY SAND 10 35 31 Boring terminated at 40 feet 7 GROUNDWATER DURING DRILLING: NOT ENCOUNTER																	
27.5 30.0 31.0 32.5 CL Firm gray LEAN CLAY with sand 33.40 20 20 85 33.0 34.0 35.0 36.0 37.5 38.0 39.0 30.0	-22.5																
32.5- CL Firm gray LEAN CLAY with sand 33.40 20 20 85 37.5- SC-SM Medium dense gray SILTY CLAYEY SAND 10 35 31 31 Boring terminated at 40 feet DEPTH OF BORING: 40 FEET \$\frac{7.5}{45.0}\$ \$\frac{7.5}{45.0	-25.0						38								0.45	0.23	82
32.5 CL Firm gray LEAN CLAY with sand 33 40 20 20 85 37.5 SC-SM Medium dense gray SILTY CLAYEY SAND 10 35 31 Boring terminated at 40 feet 42.5 SO.0 DEPTH OF BORING: 40 FEET ▼ GROUNDWATER DURING DRILLING: NOT ENCOUNTER	20.0																
30.0 32.5 CL Firm gray LEAN CLAY with sand 33 40 20 20 85 37.5 SC-SM Medium dense gray SILTY CLAYEY SAND 10 35 31 Boring terminated at 40 feet 42.5 45.0 DEPTH OF BORING: 40 FEET © GROUNDWATER DURING DRILLING: NOT ENCOUNTER	27.5																
32.5 CL Firm gray LEAN CLAY with sand 33 40 20 20 85 37.5 SC-SM Medium dense gray SILTY CLAYEY SAND 10 35 31 Boring terminated at 40 feet 45.0 Boring terminated at 40 feet DEPTH OF BORING: 40 FEET	20.0						32								0.65		
33. 40 20 20 85 35.0-37.5-38. SC-SM Medium dense gray SILTY CLAYEY SAND 10 35 31 Boring terminated at 40 feet DEPTH OF BORING: 40 FEET \$\text{GROUNDWATER DURING DRILLING: NOT ENCOUNTER}\$	-30.0			П													
35.0 SC-SM Medium dense gray SILTY CLAYEY SAND 10 35 31	-32.5		CL	H	Firm gray LEAN CLAY with sand												
37.5- SC-SM Medium dense gray SILTY CLAYEY SAND 10 35 31 Boring terminated at 40 feet 42.5- 47.5- 50.0- DEPTH OF BORING: 40 FEET FOR DEPTH OF BORING: 40 FEET FOR DEPTH OF BORING: 40 FEET FOR DEPTH OF BORING: 40 FEET							33	40	20	20	85						
37.5- SC-SM Medium dense gray SILTY CLAYEY SAND 10 35 31 Boring terminated at 40 feet 42.5- 47.5- 50.0- DEPTH OF BORING: 40 FEET \$\times \text{gray SILTY CLAYEY SAND}} \$\text{SC-SM Medium dense gray SILTY CLAYEY SAND}} 10 35 31 \$\text{31} \$\text{GROUNDWATER DURING DRILLING: NOT ENCOUNTER}\$	35.0			П													
SAND 10 35 31 Boring terminated at 40 feet 42.5- 45.0- DEPTH OF BORING: 40 FEET	-		SC-SI	vi l	Medium dense gray SILTY CLAYEY							 					
42.5- 47.5- DEPTH OF BORING: 40 FEET	16 18:			M		10	35				31						
DEPTH OF BORING: 40 FEET	40.0	<u> </u>		H	Boring terminated at 40 feet							 					
DEPTH OF BORING: 40 FEET	09 42 5																
DEPTH OF BORING: 40 FEET	42.3																
DEPTH OF BORING: 40 FEET	9 45.0																
© DEPTH OF BORING: 40 FEET ☑ GROUNDWATER DURING DRILLING: NOT ENCOUNTER	- PSI																
© DEPTH OF BORING: 40 FEET ☑ GROUNDWATER DURING DRILLING: NOT ENCOUNTER	변 - 47.5	•															
© DEPTH OF BORING: 40 FEET ☑ GROUNDWATER DURING DRILLING: NOT ENCOUNTER	9-50.0																
	M DEE	TH O	F RO	BIN	IG: 40 FFFT						07.5		10.55			EN C	
NOTE: ▼ DELAYED GROUNDWATER: N / A	()																JNTER
	MOT	E:								_						-	

KEY TO TERMS AND SYMBOLS USED ON LOGS





☐ GROUNDWATER DURING
☐ DRILLING
☐ GROUNDWATER UPON
☐ COMPLETION

UNIFIED SOIL CLASSIFICATION SYSTEM - ASTM D 2487 (1980)

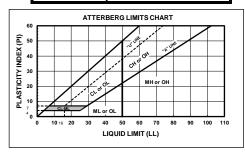
	MAJO DIVISIO		LETTER SYMBOL	TYPICAL DESCRIPTIONS
	GRAVEL &	CLEAN GRAVEL	GW	WELL-GRADED GRAVEL, GRAVEL-SAND MIXTURES WITH LITTLE OR NO FINES
COARSE- GRAINED	GRAVELLY SOILS LESS THAN 50% PASSING NO. 4 SIEVE	(LITTLE OR NO FINES)	POORLY GRADED GRAVEL, GRAVEL-SAND MIXTURES WITH LITTLE OR NO FINES	
SOILS LESS	NO. 4 SILVE	WITH APPRECIABLE	GM	SILTY GRAVEL, GRAVEL-SAND-SILT MIXTURES
THAN 50% PASSING		FINES	GC	CLAYEY GRAVELS, GRAVEL-SAND-CLAY MIXTURES
NO. 200 SIEVE		CLEAN SANDS (LITTLE OR	SW	WELL-GRADED SAND
	SANDS MORE THAN	NO FINES)	SP	POORLY-GRADED SANDS
	50% PASSING NO. 4 SIEVE	WITH APPRECIABLE	SM	SILTY SANDS
		FINES	SC	CLAYEY SANDS
			ML	INORGANIC SILTS & VERY FINE SANDS, CLAYEY SILT W/ LOW PLASTICITY INDEX
FINE- GRAINED		AND CLAYS D LIMIT < 50	CL	INORGANIC LEAN CLAYS GRAVELLY, SANDY, OR SILTY LEAN CLAYS
SOILS MORE			OL	ORGANIC SILTS & ORGANIC SILTY CLAYS W/LOW PLASTICITY INDEX
THAN 50% PASSING NO. 200 SIEVE			МН	INORGANIC SILTS W/ HIGH PLASTICITY INDEX, ELASTIC SILTS
	SILTS AND CLAYS LIQUID LIMIT ≥ 50			INORGANIC FAT CLAYS GRAVELLY, SANDY, OR SILTY FAT CLAYS
				ORGANIC CLAYS OF MED TO HIGH PLASTICITY, ORGANIC SILTS
	HIGHLY ORGAN	IC SOIL	PT	PEAT AND OTHER HIGHLY ORGANIC SOILS
	UNCLASSIFIED FILL	MATERIALS		ARTIFICIALLY DEPOSITED AND OTHER UNCLASSIFIED SOILS AND MAN-MADE SOIL MIXTURES

CONSISTENCY OF COHESIVE SOILS

	SHEAR STRENGTH
CONSISTENCY	IN TONS/FT ²
VERY SOFT	0 TO 0.125
SOFT	0.125 TO 0.25
FIRM	0.25 TO .50
STIFF	0.50 TO 1.00
VERY STIFF	1.00 TO 2.00
HARD	> 2.00 OR 2.00+

RELATIVE DENSITY - GRANULAR SOILS

CONSISTENCY	N-VALUE (BLOWS/FOOT)
VERY LOOSE	0-4
LOOSE	4-9
MEDIUM DENSE	10-29
DENSE	30-49
VERY DENSE	> 50 OR 50+



ABBREVIATIONS

HP - HAND PENETROMETER UC - UNCONFINED COMPRESSION TEST
TV - MINIATURE TORVANE UU - UNCONSOLIDATED UNDRAINED TRAIXIAL

FV - FIELD TORVANE CU - CONSOLIDATED UNDRAINED

NOTE: BORING LOGS INDICATE SHEAR STRENGTH AS OBTAINED BY ABOVE TESTS

CLASSIFICATION OF GRANULAR SOILS

U.S. STANDARD SIEVE SIZE(S)



